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## DESCRIPTION

INTERMITTENT INJECTION AEROSOL PRODUCT FOR SKIN

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## TECHNICAL FIELD

The present invention relates to an intermittent injection aerosol product for a skin. More particularly, the present invention relates to an intermittent injection aerosol product for a skin in which an injection time and a stop time are repeated at a specific ratio when an injection button is operated, thereby intermittently injecting a content to a skin including a head skin accurately.

## BACKGROUND ART

Conventionally, an injection device includes an aerosol product and a pump product. In the aerosol product, a concentrate and a propellant are filled in a pressure container and continuously carries out injection when a valve is released. The manner of injection of the aerosol product is generally continuous injection, while quantitative injection or intermittent injection is carried out depending on the use and purpose. The aerosol product for the continuous injection is suitably used for injecting a large amount of aerosol in a space or onto a wall surface. In the case in which the aerosol is continuously injected onto a skin, a large amount of liquid drips on the injection surface if a concentrate is blended in a large amount, and cooling properties are so great as to feel a pain if the propellant (liquefied gas) is blended in a large amount. The aerosol product to be quantitatively injected is suitably used for a product

having a determined effective component amount which can be utilized at each time for medical and pharmaceutical products or the like, and has no problem about the liquid dripping and the cooling properties. However, in the case in which the effective component  
5 amount to be required is large or a massage effect is to be obtained through the energy of the injection, an injection button needs to be pressed many times.

In the aerosol product for the intermittent injection, injection and stop are repeated. In the case in which the aerosol  
10 product is used for a human body, stimulation is repeated many times through the energy of the injection and the massage effect can be obtained in addition to the effect of medicament.

Depending on an injection time and a stop time, however, a feeling of stimulation is too great or too small, which is not preferable.  
15 In particular, preferable injection and stop times are varied depending on an aerosol composition.

On the other hand, the pump product can be injected in a predetermined amount by operating a finger push button for each injection. In the same manner as in the aerosol product for  
20 quantitative injection, however, it is necessary to operate a pump many times in order to obtain the massage effect through the energy of the injection. Consequently, a great deal of time and labor is required. Moreover, the pump requires a time for accumulating a pressure to some degree in order to carry out the injection. Therefore,  
25 it is hard to carry out the intermittent injection at a small interval.

In consideration of the above-mentioned circumstances, it is an object of the present invention to provide an intermittent

injection aerosol product for a skin in which an injection time and a stop time are repeated at a specific ratio when an injection button is operated, thereby intermittently injecting a content onto a skin including a head skin accurately and obtaining an excellent massage  
5 effect.

#### DISCLOSURE OF INVENTION

An intermittent injection aerosol product for a skin of the present invention is characterized in that a ratio of an injection time to  
10 a stop time is set to 0.1 to 5.0 when an injection button is operated.

Moreover, an intermittent injection aerosol product for a skin of the present invention is characterized in that the product contains 20 to 70 % by weight of a liquefied gas in an aerosol composition, and that a ratio of an injection time to a stop time is 0.1  
15 to 5.0 when an injection button is operated.

Furthermore, an intermittent injection aerosol product for a skin of the present invention is characterized in that the product contains 0.1 to 5 % by weight of a compressed gas in an aerosol composition, and that a ratio of an injection time to a stop time is 0.1  
20 to 2.0 when an injection button is operated.

#### BRIEF DESCRIPTION OF DRAWINGS

Fig. 1 is a partial sectional view showing an intermittent injection aerosol product for a skin according to an embodiment of the  
25 present invention, Fig. 2 is a view illustrating the operation of an intermittent injection mechanism in an aerosol device shown in Fig. 1, Fig. 3 is a view illustrating a method of measuring an injection time

and a stop time, and Fig. 4 is a view illustrating an injection track and the measurement of the injection time and the stop time.

#### BEST MODE FOR CARRYING OUT THE INVENTION.

5           In an intermittent injection aerosol product for a skin according to the present invention, a ratio of an injection time to a stop time is 0.1 to 5.0, and preferably, 0.5 to 4.0. When the ratio of the injection time to the stop time is 0.1 to 5.0, stimulation caused by the energy of injection and stop are properly repeated when an aerosol  
10 composition is injected onto a skin. Consequently, an excellent massage effect can be obtained. On the other hand, when the ratio of the injection time to the stop time is less than 0.1, the stop time is long or the injection time is short. Therefore, there is a problem that a long time is required for injecting a predetermined amount of  
15 medicament or a massage effect is reduced. Moreover, when the ratio of the injection time to the stop time is more than 5.0, the stop time is short or the injection time is long. Therefore, a state close to continuous injection is brought and supercooling cannot be prevented.

20           In the case of an aerosol product containing 20 to 70 % by weight of a liquefied gas in an aerosol composition, furthermore, it is preferable that the ratio of the injection time to the stop time is 0.1 to 5.0, and furthermore, 0.1 to 4.5. Within such a range, supercooling can be prevented from being caused by vaporization heat of the  
25 liquefied gas and a feeling of refreshment can be obtained by proper cooling. When the ratio of the injection time to the stop time is less than 0.1, the stop time is long or the injection time is short.

Therefore, the vaporization heat quantity of the liquefied gas is small and a proper feeling of cooling cannot be obtained. On the other hand, when the ratio is more than 5.0, the injection time is long or the stop time is short. Therefore, the vaporization heat quantity of the liquefied gas is too large so that the supercooling is caused to feel a pain.

Moreover, when the amount of the liquefied gas contained in the aerosol composition is less than 20 % by weight, mist-like injection is hard to perform and liquid dripping is increased over an injection surface. Moreover, if the aerosol composition is homogeneous, the pressure of the product is reduced. Therefore, pressure accumulation in a pressure chamber which will be described below is delayed and the ratio of the injection time to the stop time easily becomes less than 0.1. Moreover, even if the ratio of the injection time to the stop time is 0.1 to 5.0, both the injection time and the stop time are increased, and injection in a short cycle is not carried out, for example, one cycle or more is not set for one second. In some cases, therefore, the massage effect is reduced.

On the other hand, when the amount of the liquefied gas is more than 70 % by weight in the aerosol composition, a feeling of cooling is too increased so that a feeling of use is deteriorated. Moreover, since the pressure of the product is raised, the stop time is shortened and the ratio of the injection time to the stop time easily exceeds 5.0. Further, even if the ratio of the injection time to the stop time is 0.1 to 5.0, both the injection time and the stop time are shortened and a cycle of injection and stop exceeds 25 times for one second so that the state close to the continuous injection is brought.

In the case of an aerosol product containing 0.1 to 5 % by weight of a compressed gas in the aerosol composition, it is preferable that the ratio of the injection time to the stop time is 0.1 to 2.0, and furthermore, 0.2 to 1.5. Within such a range, liquid dripping over an  
5 injection surface can be prevented. Thus, the feeling of use can be more excellent than that in a conventional aerosol product using the compressed gas, and furthermore, a massage effect can be obtained. When the ratio of the injection time to the stop time is less than 0.1, the massage effect is reduced. When the ratio exceeds 2.0, the liquid  
10 dripping is caused easily.

When the amount of the compressed gas contained in the aerosol product is less than 0.1 % by weight, the pressure of the product is dropped. Therefore, the pressure accumulation in the pressure chamber is delayed and the ratio of the injection time to the  
15 stop time easily becomes less than 0.1. In the case of the compressed gas, moreover, the pressure of the product is reduced with the injection. In some cases, consequently, the injection cannot be carried out when the amount of the aerosol composition in the aerosol container is decreased.

20 Moreover, even if the ratio of the injection time to the stop time is 0.1 to 2.0, both the injection time and the stop time are increased and the injection cannot be carried out in a short cycle, for example, a cycle of three times or more for one second is not set. In some cases, therefore, the massage effect is reduced.

25 On the other hand, when the amount of the compressed gas contained in the aerosol composition exceeds 5 % by weight, the pressure of the product is raised. Therefore, the pressure

accumulation in the pressure chamber is carried out quickly and the ratio of the injection time to the stop time easily exceeds 2.0.

Moreover, even if the ratio of the injection time to the stop time is 0.1 to 2.0, both the injection time and the stop time are shortened. For example, a cycle is set to 20 times or more for one second and the state close to the continuous injection is brought.

The aerosol composition to be used in the present invention includes a concentrate containing an effective component and a propellant. In the concentrate, the effective component is dissolved or dispersed in a solvent and other components are added thereto corresponding to the configuration of a product or uses. The aerosol product is used for a product for a human body (for a skin and a head skin). More specifically, the aerosol product is used for a skin care, a cleansing agent, a moisturizing agent, a deodorizer, an aromatic, an anodyne and antiphlogistic, an astringent, an antipruritic, a tonic, a repellent and the like.

0.1 to 20 % by weight of the effective component is contained in the aerosol composition. If the amount is less than 0.1 % by weight, a desirable effect cannot be obtained and the amount of injection is increased to obtain a necessary amount. If the amount is more than 20 % by weight, further blending does not influence the effect.

In the case in which the propellant is a liquefied gas, it is contained in an amount of 20 to 70 % by weight. If the amount is less than 20 % by weight, it is hard to carry out the injection with a mist. If the amount is more than 70 % by weight, a feeling of cooling is too increased and a feeling of use becomes poor. Moreover, since

injection particles are too small, they easily scatter over the skin or the head skin and a user might suck the particles, which is not preferable.

On the other hand, in the case in which the propellant is a compressed gas, it is contained in an amount of 0.1 to 5 % by weight.

- 5 If the amount is less than 0.1 % by weight, the pressure of a product is small and the injection cannot be completed. If the amount is more than 5 % by weight, the pressure of the product is too increased, which might be dangerous.

- 10 If the propellant is the liquefied gas, the pressure of the product is 0.2 to 0.7 MPa (25°C). If the pressure is less than 0.2 MPa, the stop time is long and the ratio of the injection time to the stop time cannot be set to be a predetermined ratio. If the pressure is more than 0.7 MPa, the continuous injection is easily carried out. Moreover, there is a possibility that the pressure might exceed 0.8  
15 MPa at 35°C, which deviates from the condition of exempt from the application of the high pressure gas safety law.

- On the other hand, in the case in which the propellant is the compressed gas, the pressure is 0.2 to 1.0 MPa (25°C). If the pressure is less than 0.2 MPa, the stop time is long and the ratio of the  
20 injection time to the stop time cannot be set to be a predetermined ratio. Moreover, when the contents are decreased, the injection cannot be completed. If the pressure is more than 1.0 MPa, the continuous injection is easily carried out.

- The effective component includes a moisturizing agent, an  
25 ultraviolet absorber, a skin softener, amino acid, vitamins, hormones, an antioxidant, various extracted solutions, a fungicide and antiseptic, a deodorant, an antiperspirant, an anodyne and antiphlogistic, a

refrigerant, an astringent, an anti-inflammatory, a local anesthetic, an antihistaminics, a whitening agent, chemicals for a tonic, a repellent, a perfume and the like.

5 The moisturizing agent includes polyethylene glycol, propylene glycol, glycerin and the like.

The ultraviolet absorbent includes benzoic acid such as paraaminobenzoate or monoglycerine ester paraaminobenzoate, anthranilic acid such as methyl anthranilate, and the like.

The skin softener includes urea and the like.

10 The amino acid includes neutral amino acid such as glycine, acidic amino acid such as aspartic acid, basic amino acid such as arginine and the like.

The vitamins include vitamin A oil, retinol, retinol palmitate, acetic acid dl- $\alpha$ -tocopherol and the like.

15 The hormones include elastoradiol, ethynyl elastoradiol and the like.

The antioxidant includes ascorbic acid,  $\alpha$ -tocopherol, dibutylhydroxytoluene and the like.

20 The various extracted solutions include houttuynia extract, phellodendron bark extract, sweet clover extract, placental extract and the like.

The fungicide and antiseptic includes ester paraoxybenzoate, benzoic acid, sodium benzoate and the like.

25 The deodorant includes lauryl methacrylate, geranyl crotonate, acetophenone myristate, a green tea extracted solution and the like.

The antiperspirant includes chlorhydroxy aluminum, zinc

oxide, aluminum chloride and the like.

The anodyne and antiphlogistic includes methyl salicylate, camphor, diphenhydramine and the like.

The refrigerant includes 1-menthol, camphor and the like.

5       The astringent includes zinc oxide, allantoin hydroxyaluminum, tannic acid and the like.

The anti-inflammatory includes allantoin, glythyl retinate, azulene and the like.

10       The local anesthetic includes dibucaine hydrochloride, tetracaine hydrochloride, lidocaine hydrochloride and the like.

The antihistaminics includes diphenhydramine hydrochloride, chlorfemiramine maleate and the like.

The whitening agent includes arbutin, kojic acid and the like.

15       The chemicals for tonic include a blood circulation accelerator such as swertia herb extract, a local stimulant such as capsicum tincture, a hairy root activator such as pantothenic acid and the like.

20       The repellent includes N, N-diethyl-m-toluamide (deet), diethylamide caprylate and the like.

The propellant includes liquefied petroleum gas (butane, propane and their mixture), a liquefied gas such as dimethyl ether, tetrafluoroethane or difluoroethane, and a compressed gas such as a nitrogen gas, carbon dioxide, compressed air, or a dinitrogen  
25       monoxide gas.

Other components include a surfactant such as sorbitan fatty acid ester, glycerin fatty acid ester or decaglycerin fatty acid

ester; ester oil such as isopropyl myristate, cetyl octanate or octyldodecyl myristate; silicone such as dimethyl polysiloxane, methylphenyl polysiloxane or methylhydrogen polysiloxane; oils and fats such as avocado oil, camellia oil or turtle oil; higher fatty acid  
5 such as lauric acid, myristic acid or palmitic acid; wax such as beeswax, lanolin or lanolin acetate; higher alcohol such as lauryl alcohol, cetyl alcohol or stearyl alcohol; a high molecular compound such as agar, casein or dextrin; powder such as talc, silica, zinc oxide or titanium oxide; a pH regulator such as lactic acid, citric acid or  
10 glycolic acid, and the like.

The solvent includes water such as purified water or ion-exchange water, lower alcohol such as ethanol, propanol or isopropanol, polyhydric alcohol such as glycerin, ethylene glycol, propylene glycol or 1,3-butyleneglycol, hydrocarbon such as  
15 isoparaffin, liquid paraffin, normal pentane, isopentane or normal hexane, and the like.

In the present invention, an aerosol device shown in Fig. 1 can be used to set the ratio of the injection time to the stop time to be 0.1 to 5.0, for example.

20 An intermittent injection aerosol product for a skin according to the present invention will be described below with reference to the accompanying drawings.

Fig. 1 is a partial sectional view showing an intermittent injection aerosol product for a skin according to an embodiment of the  
25 present invention, and Fig. 2 is a view illustrating the operation of an intermittent injection mechanism in the aerosol product shown in Fig. 1.

As shown in Fig. 1, the aerosol product according to the embodiment of the present invention includes an intermittent injection mechanism in an injection button (push button) P attached to a valve stem 1. The intermittent injection mechanism comprises a  
5 cylinder 2 fitted in the valve stem 1, a piston 5 having an injection port 4 formed on a tip wall 3, a needle valve 6 for opening and closing the injection port 4, a second coil spring 7 for energization in such a direction as to open the needle valve 6, and a first coil spring 8 for energizing the piston 5 in such a direction as to close the needle valve  
10 6, and a regulation member 9a is provided between the tip wall 3 of the piston 5 and a tip portion 6a of the needle valve 6 and a regulation member 9b which is shorter than the second coil spring is provided on the outer periphery of the second coil spring.

In the present embodiment, such regulation members 9a  
15 and 9b are provided. Consequently, when the injection button P is operated, the injection time and the stop time are repeated at a specific ratio so that intermittent injection can be carried out accurately.

More specifically, when the regulation member 9a is  
20 provided, the positions of the inside of the piston and an O ring are fixed. Moreover, the regulation member 9b is provided so that the distance of movement of the needle valve is fixed. Consequently, a timing of valve opening and closing is stabilized. Accordingly, injection and stop can be carried out clearly and the intermittent  
25 injection can be performed accurately.

Although the materials for the regulation members 9a and 9b are not particularly limited, it is possible to use a resin such as

nylon, polyacetal or polyethylene terephthalate.

The injection button P is provided with a skirt portion 10 to surround and protect the valve stem 1, and an inlet port 11 communicating with the cylinder 2 is formed in the fitting portion of the valve stem 1. The piston 5, the needle valve 6, the second coil spring 7, the first coil spring 8 and the like are accommodated in the cylinder 2.

The cylinder 2 is divided into a large diameter portion 2a on the tip side (the left side in the drawing) and a small diameter portion 2b on the rear end side (the right side in the drawing) through a step portion 12 formed on the inside thereof, and the piston 5 and the cylindrical needle valve 6 having the tip portion 6a fitted therein through the opening of a rear end funnel-shaped portion 13 of the piston 5 are slidably inserted in the large diameter portion 2a concentrically with the cylinder 2, respectively. Moreover, a cap 14 having a hole is fastened to the outer peripheral portion of the tip of the cylinder 2 with a pin 15, and the tip portion of the piston 5 is protruded from a tip hole 16.

The piston 5 includes a tip cylindrical portion 17 and the funnel-shaped portion 13 having an inside diameter increased continuously from a middle portion, and the outer peripheral surface of the funnel-shaped portion 13 is provided airtightly in slidable contact with the inner peripheral surface of the large diameter portion 2a and the funnel-shaped portion 13 abuts on a stopper 18 fastened to the step portion 12.

The first coil spring 8 for energizing the piston 5 in a valve closing direction, that is, a rightward direction in the drawing is

wound around the outer periphery of the piston 5 in a compression state between the cap 14 and the outer peripheral step portion of the funnel-shaped portion 13 of the piston 5 in the large diameter portion 2a of the cylinder 2.

5           The needle valve 6 penetrates through the central opening of the stopper 18 with a small clearance provided therearound, and an O ring 19 for slidably coming in contact with the inner peripheral surface of the piston 5 airtightly is fitted and attached into the outer peripheral groove of the tip portion 6a. A step portion 6c is formed on  
10 a rear end 6b. By sliding the outer peripheral surface of the step portion 6c over the inner peripheral surface of the small diameter portion 2b, a stable sliding characteristic can be obtained. The clearance can be appropriately adjusted.

          The second coil spring 7 is wound around the outer  
15 periphery of the needle valve 6 in a free length state between the stopper 18 and the step portion 6c of the needle valve 6. The second coil spring 7 serves to be flexed when both the piston 5 and the needle valve 6 are moved in a leftward direction in the drawing, thereby applying energizing force to only the needle valve 6 in a valve opening  
20 direction (the rightward direction in the drawing). The second coil spring 7 is incorporated in the free length state such that the needle valve 6 can be moved together with the piston 5 while displaying a sealing function through the O ring 19 by the pressure of a content. It is possible to change and set an initial flex in relation to the  
25 selection of the spring constant of the second coil spring 7.

          In the aerosol product according to the present embodiment, consequently, the piston 5 is positioned on the

rightmost end in the drawing of a stroke through the first coil spring 8 and the inside of the cylinder 2 is set in an airtight state with respect to the outside through the O ring 19 provided between the inner peripheral surface of the piston 5 and the tip portion 6a of the needle valve 6, and the abutment of the tip face of the needle valve 6 and the regulation member 9. In this case, the inside of the cylinder 2 will be particularly referred to as a pressure chamber 20. The rear end funnel-shaped portion 13 of the piston 5 abuts on the stopper 18. The needle valve 6 is set in such a state that the rear end 6b abuts on the side wall surface of the cylinder 2. The second coil spring 7 is set in a free length state, so that force thereof is not particularly applied to the needle valve 6.

Next, the operation of the intermittent injection mechanism in the aerosol product according to the present embodiment will be described with reference to Figs. 1 and 2.

First of all, Fig. 1 shows the state (valve closing state) in which the intermittent injection mechanism does not carry out an injecting operation.

Subsequently, when the injection button P is pushed down (a direction of an arrow A), the valve stem 1 is pressed downward so that an aerosol valve (not shown) is opened, thereby the content flows into the pressure chamber 20 in the cylinder 2. As shown in Fig. 2(a), consequently, the piston 5 and the needle valve 6 are moved together in a direction of an arrow H while flexing the first and second coil springs 8 and 7 by a difference between an internal pressure applied by the content and an external air pressure. As shown in Fig. 2(b), finally, the needle valve 6 is stopped to be moved by the abutment of

the step portion 6c on the regulation member 9b. However, the first coil spring 8 is still set in a flexing state. Therefore, the piston 5 is further moved and the sealing state of the piston 5 and the needle valve 6 is released at this time so that a clearance for causing the  
5 outside to communicate with the pressure chamber 20 is generated between the piston 5 and the needle valve 6.

By the regulation member 9b, the stop position of the needle valve is always constant, and furthermore, the position of the tip (O ring) of the needle valve in a cylindrical portion of the tip of the  
10 piston is also constant. Therefore, such a timing that the sealing is released is always constant.

As shown in Fig. 2(C), subsequently, when the content is injected toward the outside through the clearance, the pressure of the pressure chamber 20 is started to be dropped such that the piston 5 is  
15 returned in the valve closing direction through the first coil spring 8 without fully injecting the content. However, the difference between a pressure on the tip side of the needle valve 6 and a pressure on the rear end side thereof is reduced simultaneously with the injection of the content. Therefore, the needle valve 6 is repelled in a direction of  
20 an arrow K through the second coil spring 7 and is thereby pushed back to a position shown in the drawing. As a result, an injection passageway for the content can be sufficiently maintained until the piston 5 is returned to the valve closing position (the position shown in Fig. 1).

25 Accordingly, the injection is continuously carried out for a constant time and the internal pressure of the pressure chamber 20 is sufficiently dropped when the piston 5 is returned to the valve closing

position. As a result, a constant time is required for recovering the internal pressure of the pressure chamber 20 to such a pressure as to generate the injection again, and the valve closing state is maintained. After the internal pressure is recovered, the content is injected again.

5 Consequently, the intermittent injection can be obtained. Moreover, the valve can also be opened or closed by sending a signal to control a driving mechanism such as a motor by using an external personal computer or the like, for example, in addition to the above-mentioned aerosol device.

10 While examples of the present embodiment will be described below, the present invention is not limited to only the following examples.

#### EXAMPLES 1 to 5

15 An aerosol composition consisting of 50 % by weight of a concentrate containing 50 % by weight of purified water and 50 % by weight of ethanol, and 50 % by weight of dimethyether (DME) to be a liquefied gas was filled in a pressure container formed of aluminum so that an aerosol product was obtained. Subsequently, the aerosol  
20 product was preserved under the condition of each temperature and an injection time and a stop time were measured by the following method.

An aerosol valve having a stem hole of  $\phi 0.3$  mm and a housing lower hole of  $\phi 0.3$  mm was used and the injection button  
25 shown in Fig. 1 was used. A spring including a first spring having a load of 480 g and a second spring having a load of 180 g was used for the injection button, and a piston hole diameter is 1.0 mm. First of

all, as shown in Fig. 3, the following is carried out.

1. A photosensitive paper 51 is applied onto the outside of a cylinder having a diameter of 300 mm.
2. The number of rotations of the cylinder is set to one rotation/second.

Accordingly, the cylinder has a circumference of  $2\pi r = 942$  mm and movement is carried out by 942 mm per second.

3. The cylinder is rotated to inject the aerosol product to be a test body in a position of a 0 point (a distance of 10 cm from the photosensitive paper). As shown in Fig. 4, in an injection track 52, an injection time  $T_1$  ( $= y/942$ ,  $y$  is a measured distance) and a stop time  $T_0$  were alternately measured. The distance is an average for five continuous times and is set to a maximum value when the measurement is carried out five times or less per second.

The result is shown in Table 1.

TABLE 1

Concentrate/ DME (weight ratio)		Ex. 1	Ex. 2	Ex. 3	Ex. 4	Ex. 5
	Preservation temperature (°C)	5	15	25	30	35
50/50	Product pressure (MPa)	0.21	0.27	0.40	0.43	0.49
	Injection time (second)	0.032	0.043	0.03	0.028	0.034
	Stop time (second)	0.224	0.088	0.023	0.013	0.008
	Injection/stop	0.14	0.49	1.30	2.15	4.25
	Cycle (times/second)	3.9	7.6	18.9	24.4	23.8

### EXAMPLES 6 to 10

The same concentrate as that in Example 1 was filled in a pressure container formed of aluminum and a nitrogen gas to be a compressed gas was filled to a predetermined product pressure shown in Table 2 to obtain an aerosol product. In the same manner, an injection time and a stop time were measured. The result is shown in Table 2.

TABLE 2

	Ex. 6	Ex. 7	Ex. 8	Ex. 9	Ex. 10
Product pressure (MPa)	0.20	0.30	0.50	0.70	0.90
Compressed gas weight (%)	0.23	0.32	0.51	0.68	0.86
Injection time (second)	0.032	0.038	0.041	0.046	0.051
Stop time (second)	0.143	0.133	0.069	0.052	0.041
Injection/stop	0.22	0.29	0.59	0.88	1.24
Cycle (times/second)	5.7	5.8	9.1	10.2	10.9

### EXAMPLES 11 to 13

An aerosol composition (Example 11) containing 60 % by weight of the same concentrate as that in Example 1 and 40 % by weight of dimethylether, an aerosol composition (Example 12) containing 70 % by weight of the same concentrate and 30 % by weight of dimethylether, and an aerosol composition (Example 13) containing 40 % by weight of the same concentrate and 60 % by weight of dimethylether were filled in a pressure container formed of aluminum. Thus, an aerosol product was obtained. The aerosol product thus

obtained was maintained at 25°C, the same injection button as that in Example 1 was attached thereto, and an injection time and a stop time were measured in the same manner. The result is shown in Table 3.

5

#### EXAMPLES 14 and 15

An aerosol composition (Example 14) containing 50 % by weight of ethanol to be a concentrate and 50 % by weight of liquefied petroleum gas having a vapor pressure of 0.35 (MPa) at 20°C, and an aerosol composition (Example 15) containing 50 % by weight of ethanol and 50 % by weight of liquefied petroleum gas having a vapor pressure of 0.40 (MPa) at 20°C were filled in a pressure container formed of aluminum so that an aerosol product was obtained. The aerosol product thus obtained was maintained at 25°C and the same injection button as that in Example 1 was attached. In the same manner, an injection time and a stop time were measured. The result is shown in the Table 3.

TABLE 3

	Ex. 11	Ex. 12	Ex. 13	Ex. 14	Ex. 15
Product pressure (MPa)	0.33	0.27	0.44	0.39	0.42
Injection time (second)	0.030	0.031	0.031	0.033	0.030
Stop time (second)	0.051	0.083	0.011	0.021	0.016
Injection/stop	0.59	0.37	2.82	1.57	1.88
Cycle (times/second)	12.3	8.8	23.8	18.5	21.7

#### COMPARATIVE EXAMPLE 1

An aerosol composition consisting of 20 % by weight of a concentrate containing 50 % by weight of purified water and 50 % by weight of ethanol and 80 % by weight of dimethylether to be a liquefied gas was filled in a pressure container so that an aerosol product was obtained. In the same manner as in Example 1, an injection time and a stop time were measured. The result is shown in Table 4.

#### COMPARATIVE EXAMPLE 2

An aerosol composition consisting of 85 % by weight of a concentrate containing 50 % by weight of purified water and 50 % by weight of ethanol and 15 % by weight of dimethylether to be a liquefied gas was filled in a pressure container so that an aerosol product was obtained. In the same manner as in Example 1, an injection time and a stop time were measured. The result is shown in Table 4.

#### COMPARATIVE EXAMPLE 3

The same concentrate as that in Example 1 was filled in a pressure container and 1.05 % by weight of a nitrogen gas was then filled as a compression gas so that an aerosol product was obtained. In the same manner as in Example 1, an injection time and a stop time were measured. The result is shown in the Table 4.

#### COMPARATIVE EXAMPLE 4

The same concentrate as that in Example 1 was filled in a pressure container and 0.18 % by weight of a nitrogen gas was then filled as a compression gas so that an aerosol product was obtained.

In the same manner as in Example 1, an injection time and a stop time were measured. The result is shown in the Table 4.

TABLE 4

	Com. Ex. 1	Com. Ex. 2	Com. Ex. 3	Com. Ex. 4
5 Product pressure (MPa)	0.45	0.14	1.10	0.15
Injection time (second)	0.038	0.028	0.092	0.022
Stop time (second)	0.005	0.336	0.018	0.245
10 Injection/stop	7.60	0.08	5.11	0.09
Cycle (times/second)	23.3	2.7	9.1	3.7

Next, a feeling of use was evaluated. A test sample in each of Examples 1 to 15 and Comparative Examples 1 to 4 was injected into an arm and the following items were evaluated. The result is shown in Tables 5 to 8.

TABLE 5

	Ex. 1	Ex. 2	Ex. 3	Ex. 4	Ex. 5
20 Feeling of stimulation	A	A	A	A	A
Feeling of cooling	A	A	A	A	A
Feeling of use	A	A	A	A	A

TABLE 6

	Ex. 6	Ex. 7	Ex. 8	Ex. 9	Ex. 10
Feeling of stimulation	A	A	A	A	A
Feeling of cooling	-	-	-	-	-
Feeling of use	A	A	A	A	A

TABLE 7

	Ex. 11	Ex. 12	Ex. 13	Ex. 14	Ex. 15
Feeling of stimulation	A	A	A	A	A
Feeling of cooling	A	A	A	A	A
Feeling of use	A	A	A	A	A

TABLE 8

	Com. Ex. 1	Com. Ex. 2	Com. Ex. 3	Com. Ex. 4
Feeling of stimulation	C	B	C	B
Feeling of cooling	C	B	-	-
Feeling of use	D	C	C	B

Feeling of stimulation

A : A good feeling of massage was obtained.

B : The energy of injection was too small and was not satisfied.

C : The energy of injection was so great as to feel a pain.

5

Feeling of cooling (only the example using a liquefied gas was evaluated)

A : A good feeling of cooling was obtained.

B : A feeling of cooling was not satisfied.

C : A feeling of cooling was so great as to feel a pain.

Feeling of use

5 A : Liquid dripping was not caused and troubles were not occurred during use.

B : A long time was required for injection in a proper amount.

C : Liquid dripping was considerably caused and convenience for use could not be obtained.

10 D : Scattering was considerably caused over an injection surface.

15 Next, the following concentrate was filled in a pressure container and a propellant was then filled. Thus, the aerosol product according to the present invention was obtained. In the same manner as in the above-mentioned examples, the characteristics of the product and the feeling of use were evaluated. The result is shown in Tables 9 and 10.

EXAMPLE 16

Tonic

<Concentrate>

	Extract of Japanese green gentian	0.5
5	Capsicum tincture	0.2
	Placental extract	0.5
	Benzalkonium chloride	0.1
	Glycol propylene	2.0
	Ester parahydroxybenzoate	0.1
10	Perfume	0.1
	Etanol	66.5
	Purified water	30.0
Total		100.0 (% by weight)

15 <Aerosol prescription>

	The above-mentioned concentrate	50.0
	Dimetylether	50.0
Total		100.0 (% by weight)

EXAMPLE 17

Cleansing agent for head skin

<Concentrate>

	Light isoparaffine	50.0
5	Sorbitan sesquiolate	1.0
	POE(2) oleylether	1.0
	Perfume	0.1
	Ethanol	30.0
	Purified water	17.9
10	Total	100.0 (% by weight)

<Aerosol prescription>

	The above-mentioned concentrate	40.0
	Dimetylether	60.0
15	Total	100.0 (% by weight)

EXAMPLE 18

Anodyne and antiphlogistic

<Concentrate>

20	Methyl salicylate	3.0
	d1-camphor	5.0
	1-menthol	5.0
	Perfume	0.1
	Ethanol	86.9
25	Total	100.0 (% by weight)

<Aerosol prescription>

The above-mentioned concentrate	50.0
Liquefied petroleum gas (0.35 MPa at 20°C)	50.0
<hr/>	
Total	100.0 (% by weight)

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EXAMPLE 19

Massage agent for foot sole

<Concentrate>

	Glyceryl glytylretinate	0.1
10	Lauryl methacrylate	0.2
	Benzalkonium chloride	0.1
	Green tea extract	0.5
	Perfume	0.1
	Ethanol	99.0
<hr/>		
15	Total	100.0 (% by weight)

<Aerosol prescription>

	The above-mentioned concentrate	60.0
	Liquefied petroleum gas (0.35 MPa at 20°C)	40.0
<hr/>		
20	Total	100.0 (% by weight)

EXAMPLE 20

Tonic

<Concentrate>

	d1- $\alpha$ -tocopheryl acetate	0.5
5	Swertia herb extract	0.5
	Pantothenic acid	0.5
	Propylene glycol	2.0
	Perfume	0.1
	Etanol	56.4
10	Purified water	40.0
Total		100.0 (% by weight)

<Aerosol prescription>

	The above-mentioned concentrate	97.5
15	Carbon dioxide	2.5
Total		100.0 (% by weight)

EXAMPLE 21

Lotion

<Concentrate>

	1,3-butylene glycol	5.0
5	Glycerin	5.0
	Oleyl alcohol	0.1
	POE(20)sorbitan monolaurate	1.0
	Phenoxy ethanol	0.1
	Etanol	10.0
10	Purified water	78.8
Total		100.0 (% by weight)

<Aerosol prescription>

	The above-mentioned concentrate	99.5
15	Nitrogen gas	0.5
Total		100.0 (% by weight)

TABLE 9

	Ex. 16	Ex. 17	Ex. 18	Ex. 19	Ex. 20	Ex. 21
Product pressure (MPa)	0.33	0.38	0.39	0.36	0.64	0.71
Injection time (second)	0.032	0.029	0.031	0.030	0.043	0.045
Stop time (second)	0.053	0.023	0.022	0.046	0.063	0.051
Injection/stop	0.60	1.26	1.41	0.65	0.68	0.82
Cycle (times/second)	11.8	19.2	18.9	13.2	9.4	10.4

TABLE 10

	Ex. 16	Ex. 17	Ex. 18	Ex. 19	Ex. 20	Ex. 21
Feeling of stimulation	A	A	A	A	A	A
Feeling of cooling	A	A	A	A	-	-
Feeling of use	A	A	A	A	A	A

#### INDUSTRIAL APPLICABILITY

According to the present invention, it is possible to  
5 intermittently inject a content into a skin including a head skin  
accurately.